

Rutting Performance Tests for Airport Asphalt Mixture Design

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Problem Statement

- A need exist to adopt a laboratory rutting performance test for airport HMA mixture design to accompany a new specification based on gyratory compaction



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Background

- Gyratory HMA mixture design methods adopted by state DOTs in the 1990s
- Airport HMA mixture design historically centered around Marshall manual compaction. Gyratory compaction option added 21 July 2014
- New regulations allow heavier loads and higher tire pressure for each category of aircraft traffic. Volumetric properties for mixture acceptance may not be sufficient to design for these standards
- No performance test for gyratory mixture design has been widely adopted



Objective

- Identify a laboratory procedure for testing HMA designed for airfield pavement that can identify mixtures prone to rutting



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Research Approach

- Subject selected HMA mixtures to suite of potential performance tests
- Establish performance testing acceptance thresholds based on laboratory data
- Validate performance thresholds using range of HMA mixtures and binder grades



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HMA Mixtures

- Phase 1

- ▶ Limestone, Granite, and Chert Gravel aggregates
- ▶ Various gradations and natural sand dosages
- ▶ 26 mixtures with PG 64-22 binder
- ▶ 8 mixtures with PG 76-22 binder

- Phase 2

- ▶ Aggregates sourced from plants producing mixtures for paving at NAPTF, Columbus AFB, and Boston Logan International and from Granite Mountain Quarry, AR
- ▶ 6 mixtures, each with 6 binders
- ▶ 2 base grades with 2&3 grade “bumps”



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Selected Performance Tests

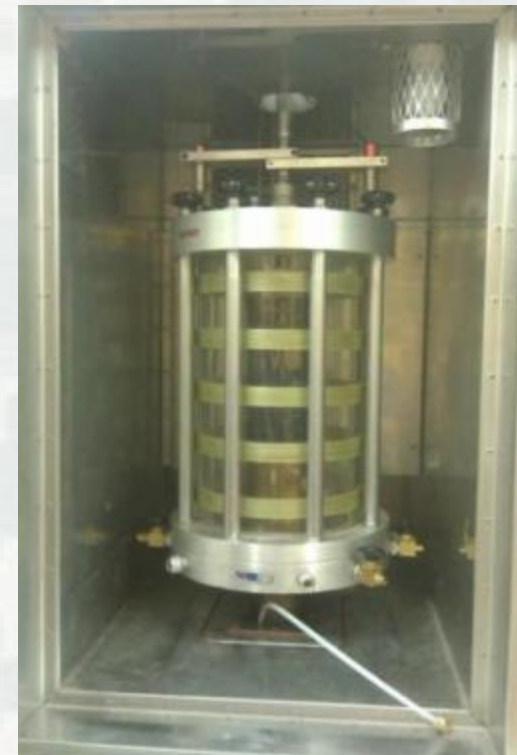
- Flow Number
 - Confined uniaxial repeated loading
- Flow Time
 - Confined uniaxial static loading
- Indirect Tensile Strength
 - Compression using Lottman breaking head
- Asphalt Pavement Analyzer
 - Simulative wheel tracking test



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Repeated Load

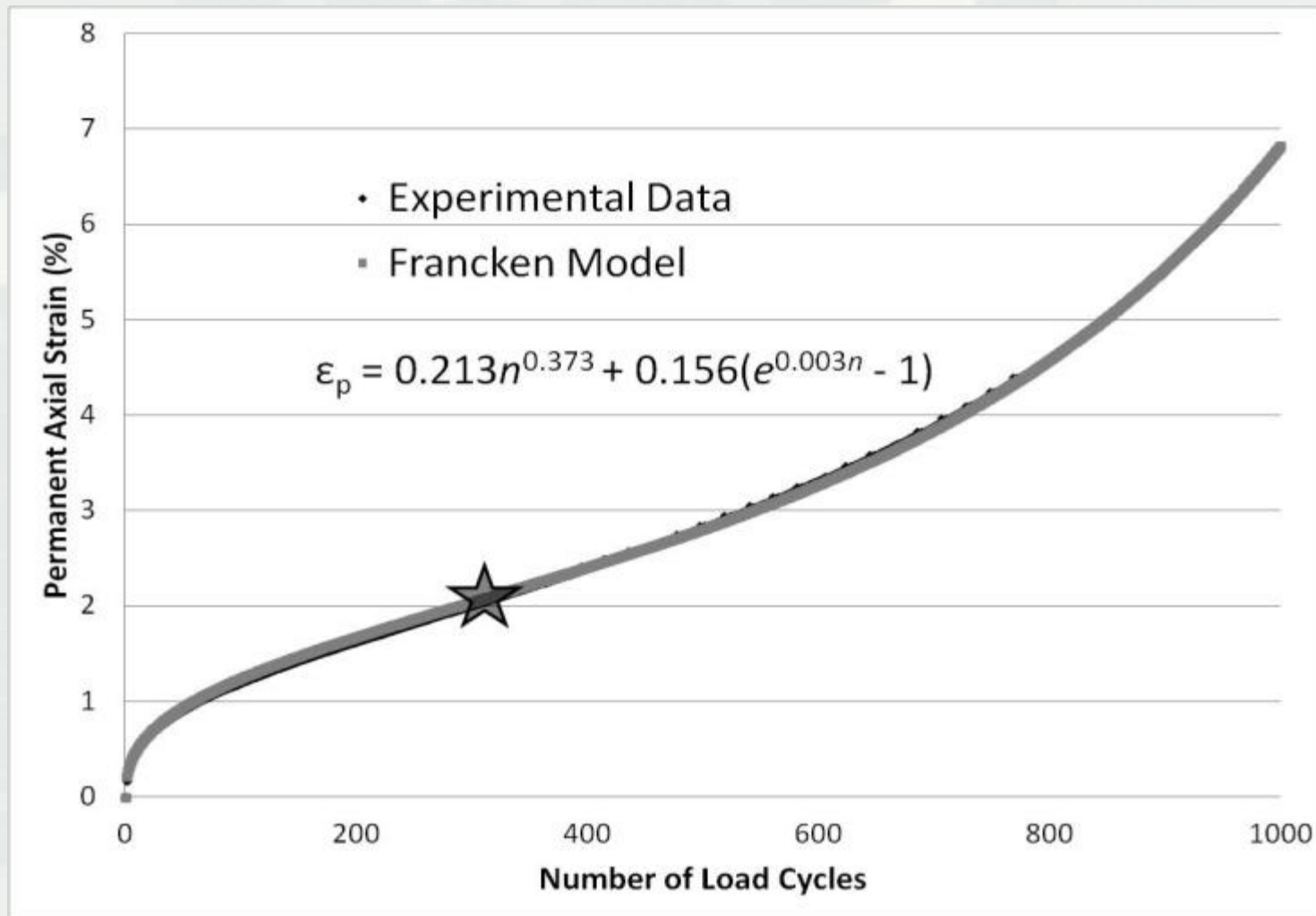
- Permanent Deformation versus Number of Load Cycles
 - 0.1 s pulse, 0.9 s rest
 - Confining pressure = 40 psi
 - Axial stress = 200 psi
 - Temp = T_{eff} (43°C or 37°C)
 - Francken model fit to data



$$\varepsilon_p = An^B + C(e^{Dn} - 1)$$

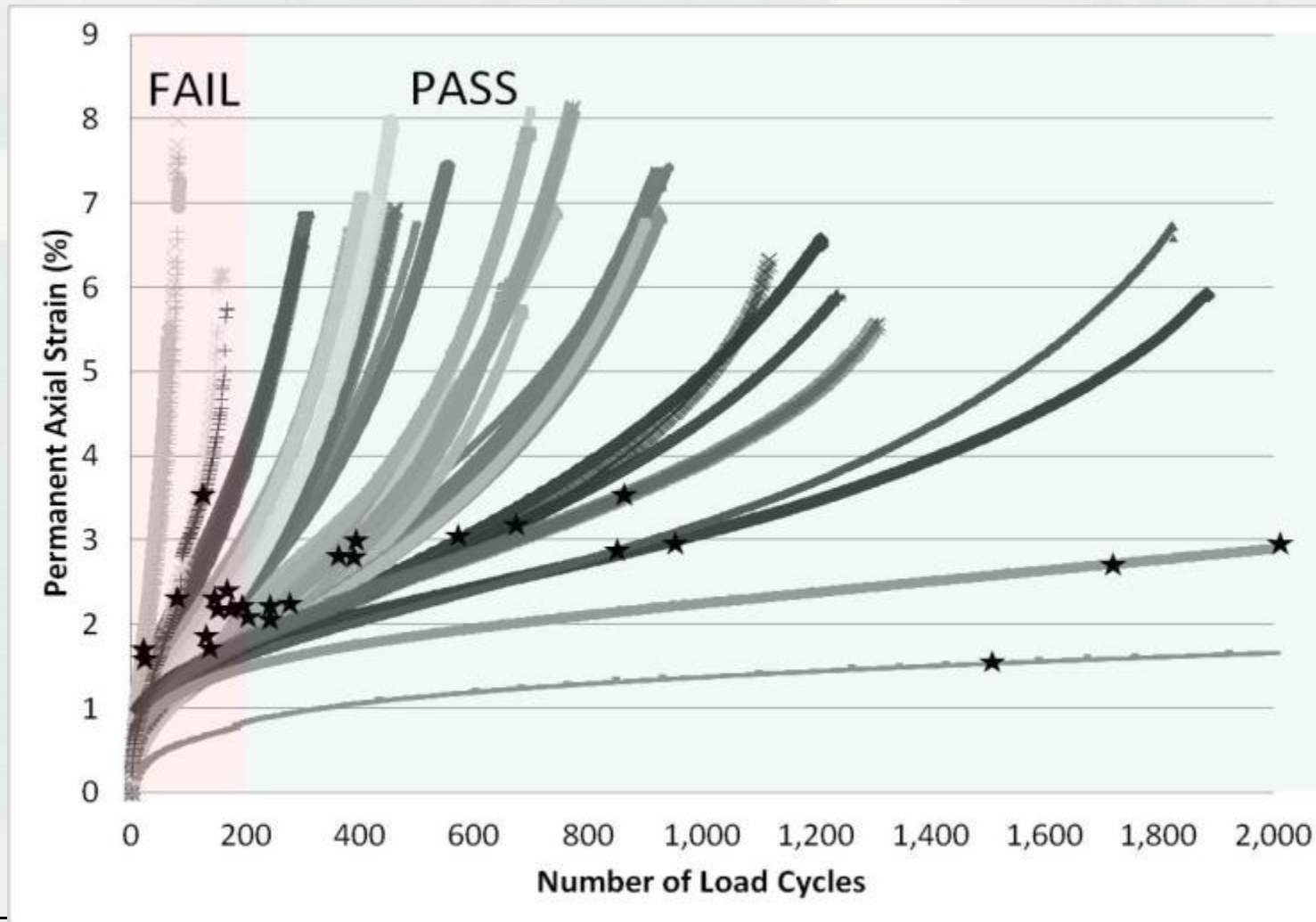


Example Repeated Load Data



Example Criterion for Flow Number

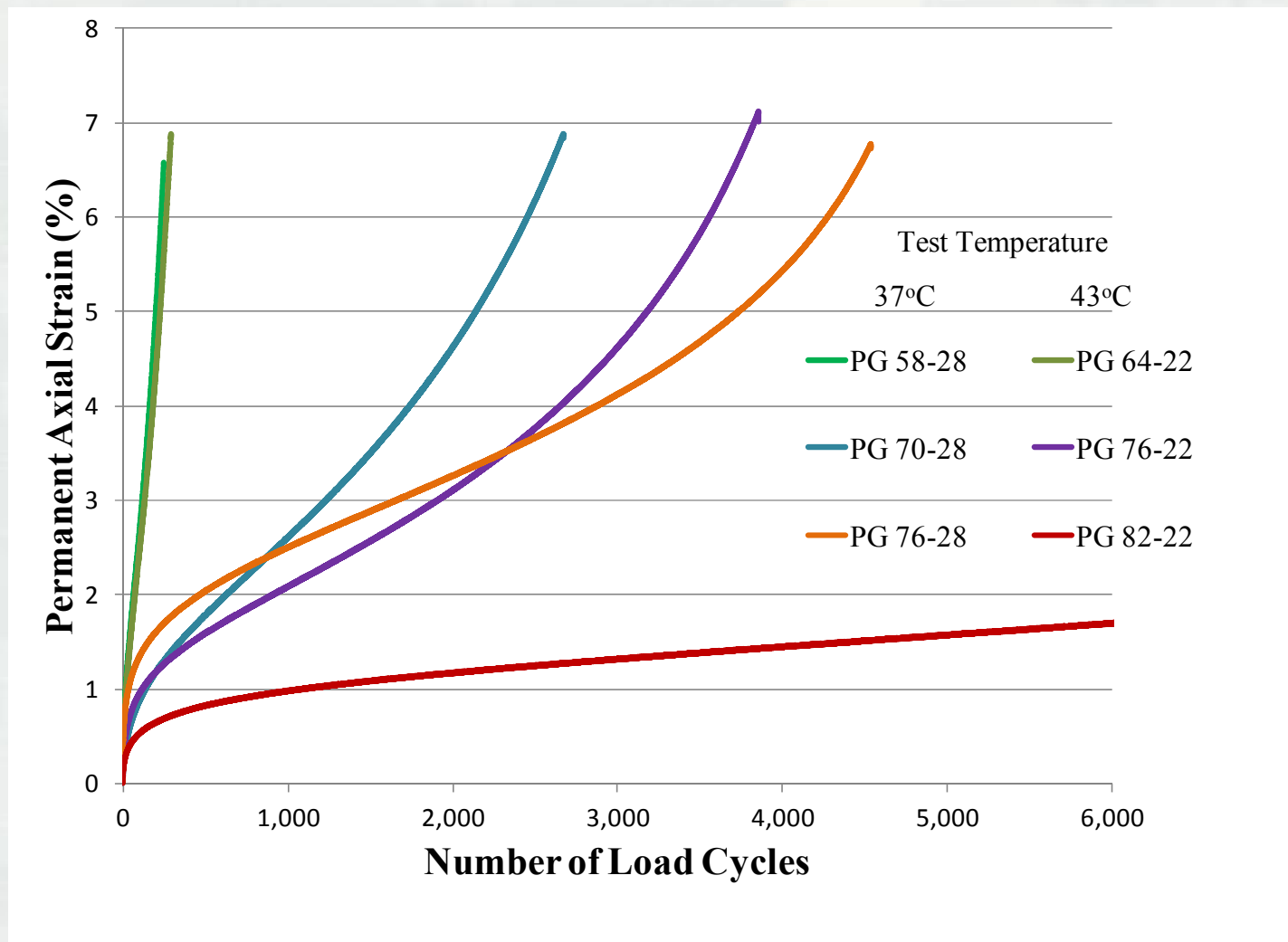
Phase 1 Results



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Influence of Binder on Flow Number

Example from Phase 2



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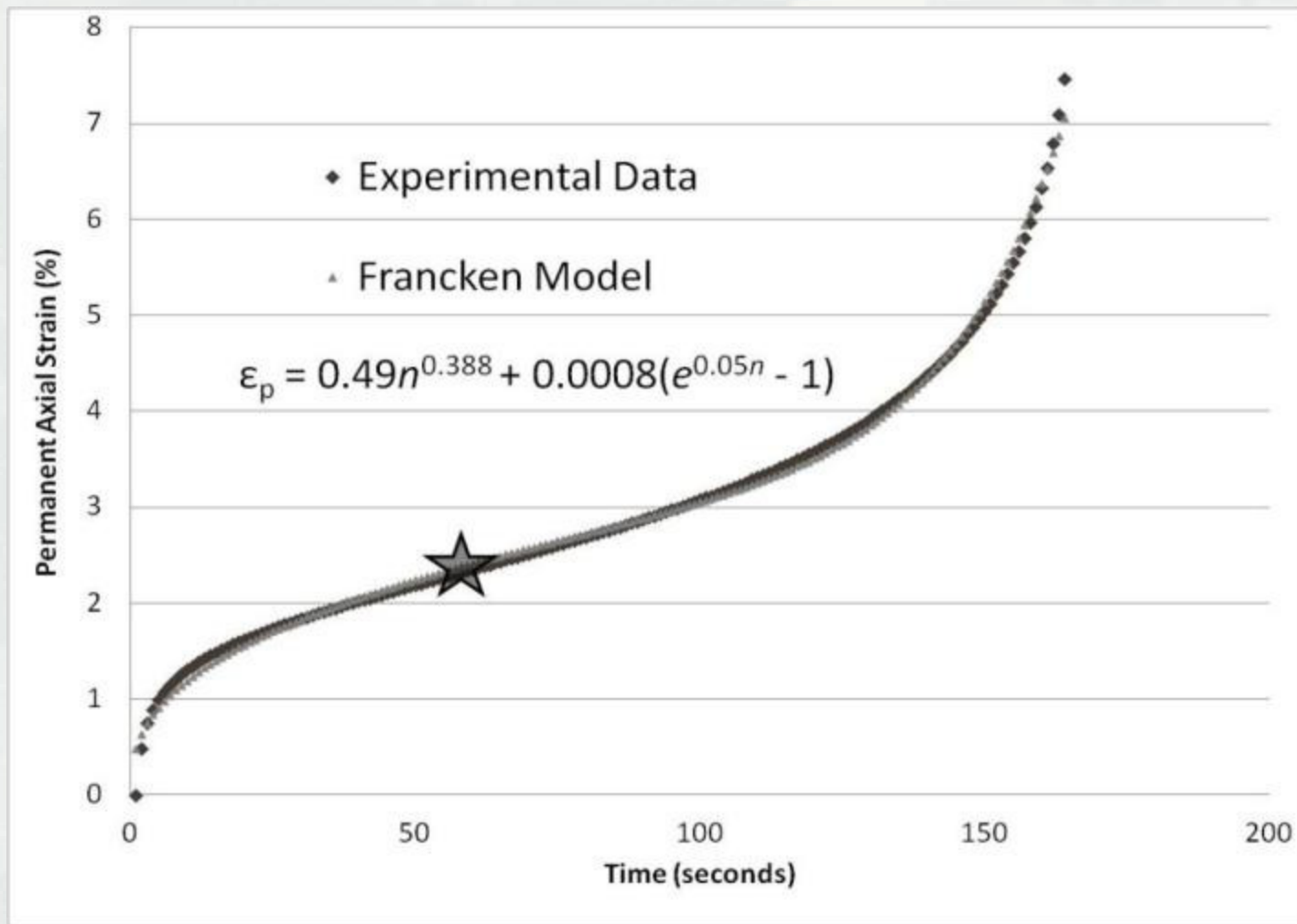
Flow Time

- Permanent Deformation versus Time (static loading condition)
 - Constant load
 - Confining pressure = 40 psi
 - Axial stress = 200 psi
 - Temp = T_{eff} (43°C or 37°C)
 - Francken model fit to data

$$\varepsilon_p = An^B + C(e^{Dn} - 1)$$



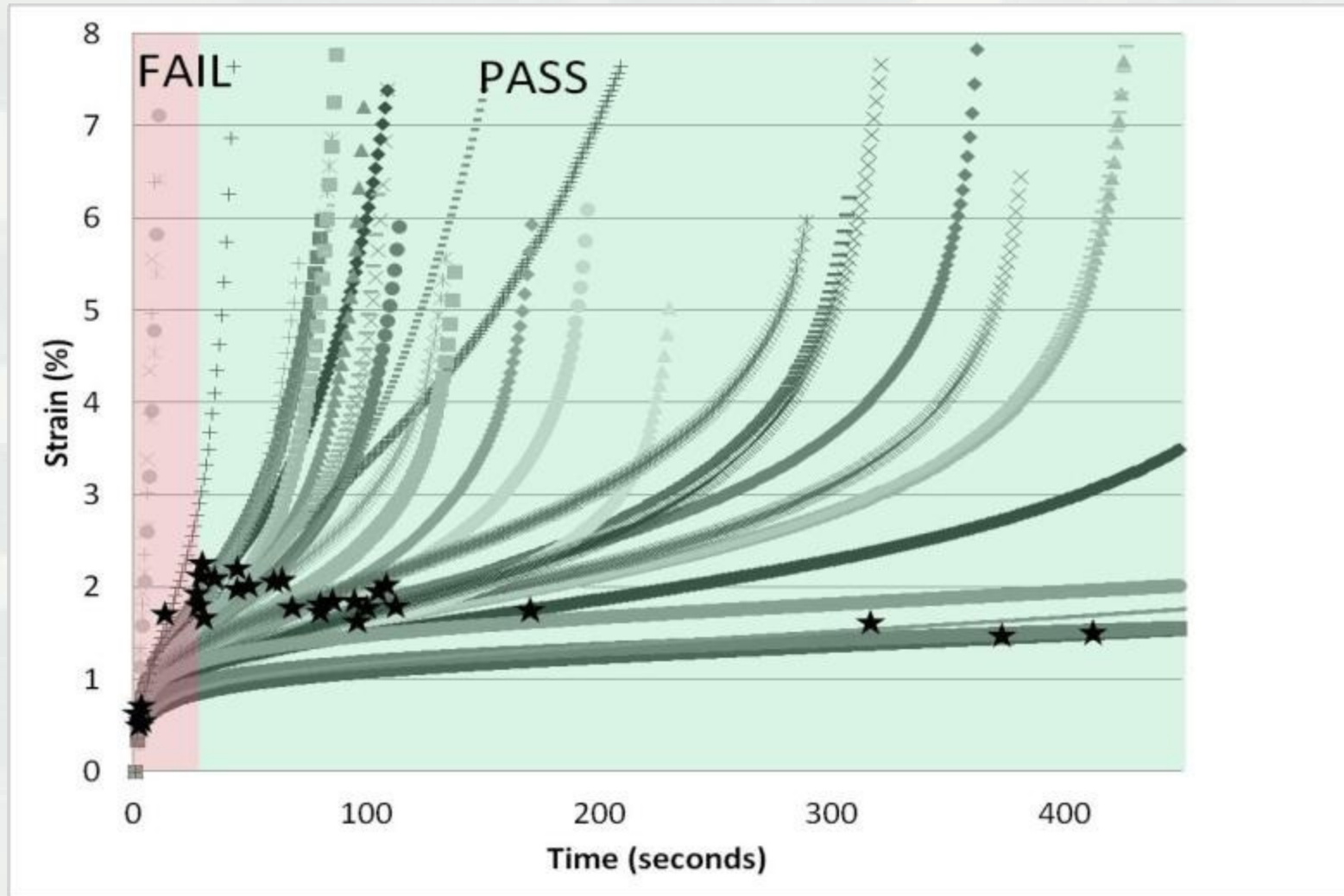
Example Static Creep Data



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Example Criterion for Flow Time

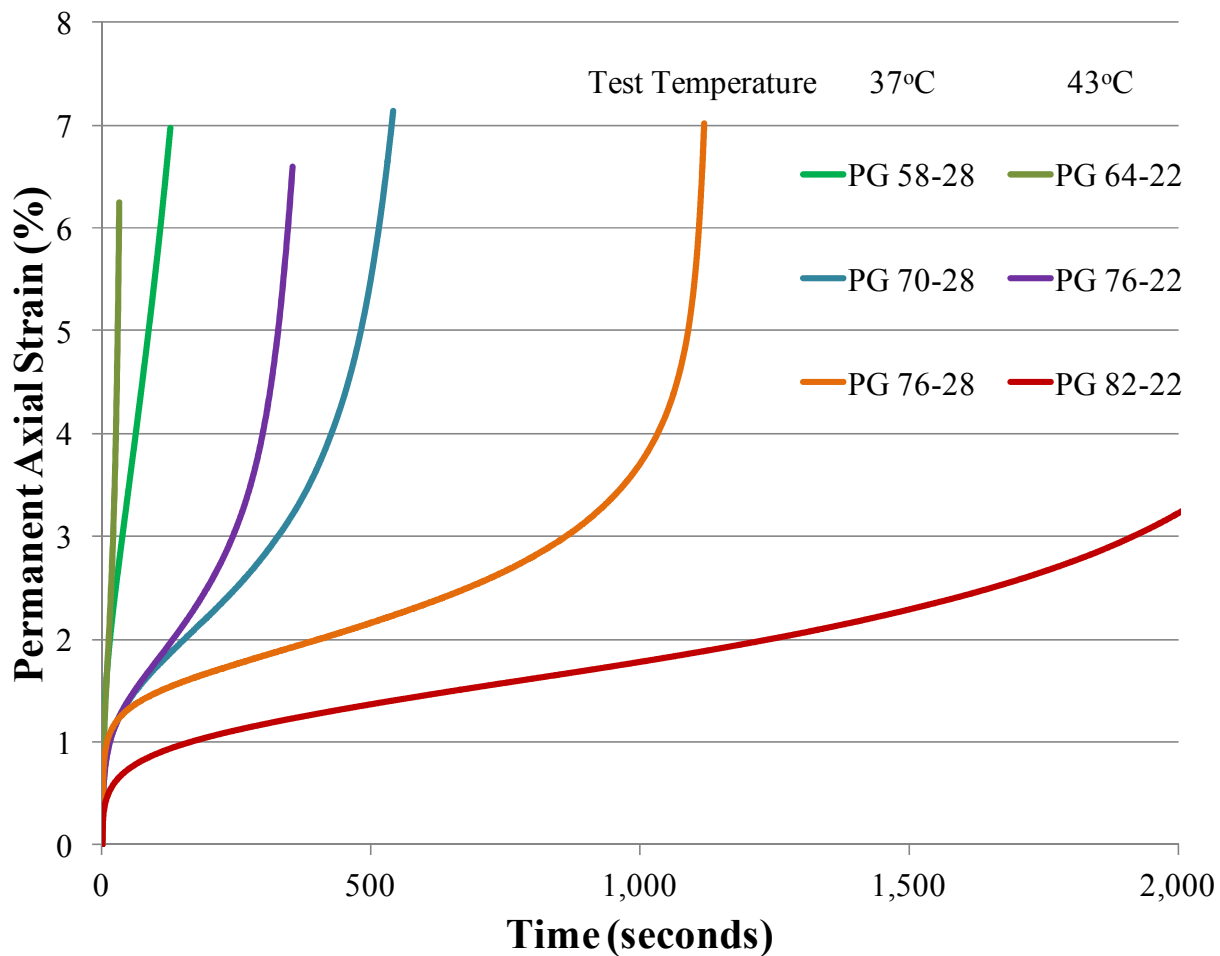
Phase 1 Results



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Influence of Binder on Flow Time

Example from Phase 2



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Asphalt Pavement Analyzer (APA)

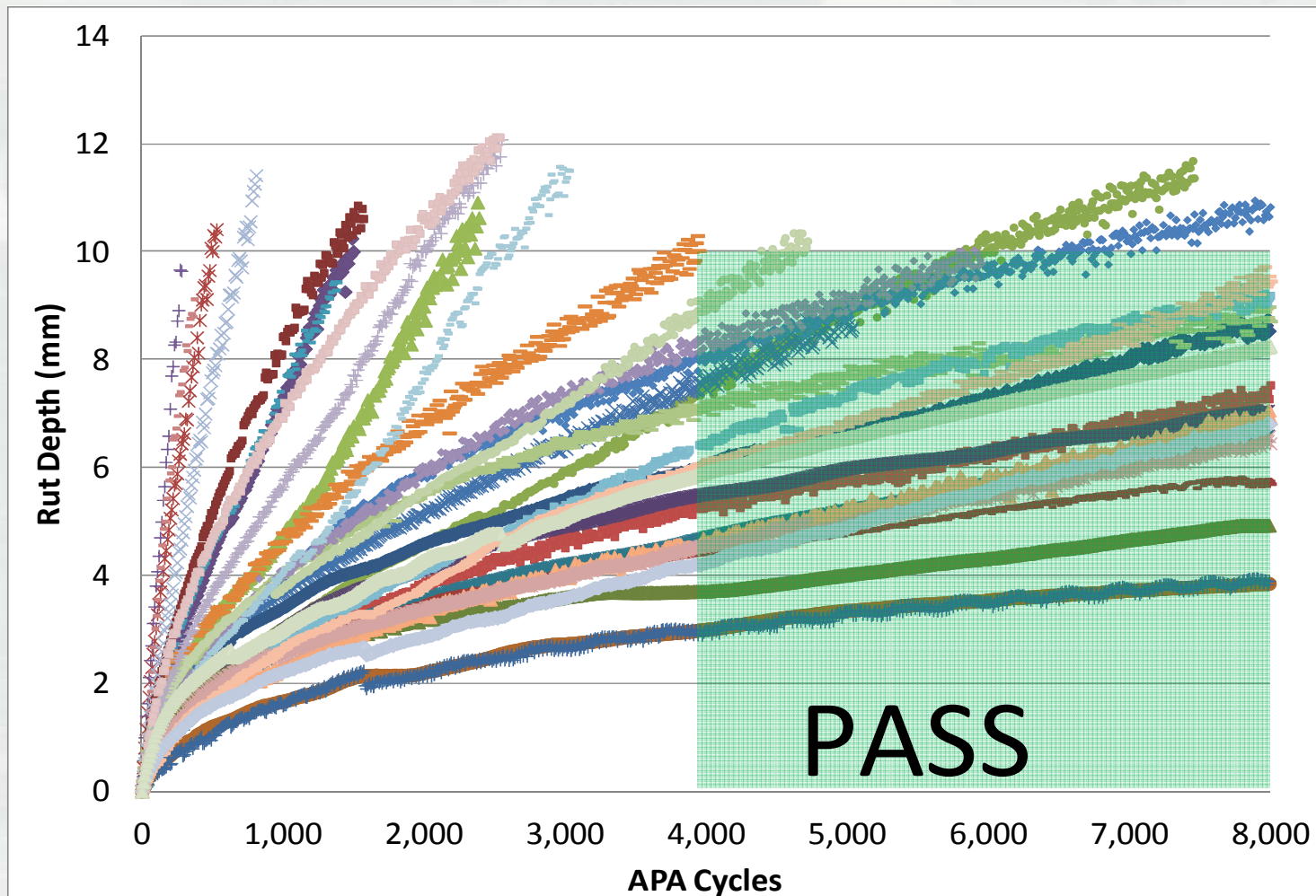
- Laboratory Wheel Tracking Device
- 250 psi hose pressure
- 8,000 cycles or failure
- Records cumulative rut depth per cycle
- Test temperature based on PG grade



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Example Criterion for APA

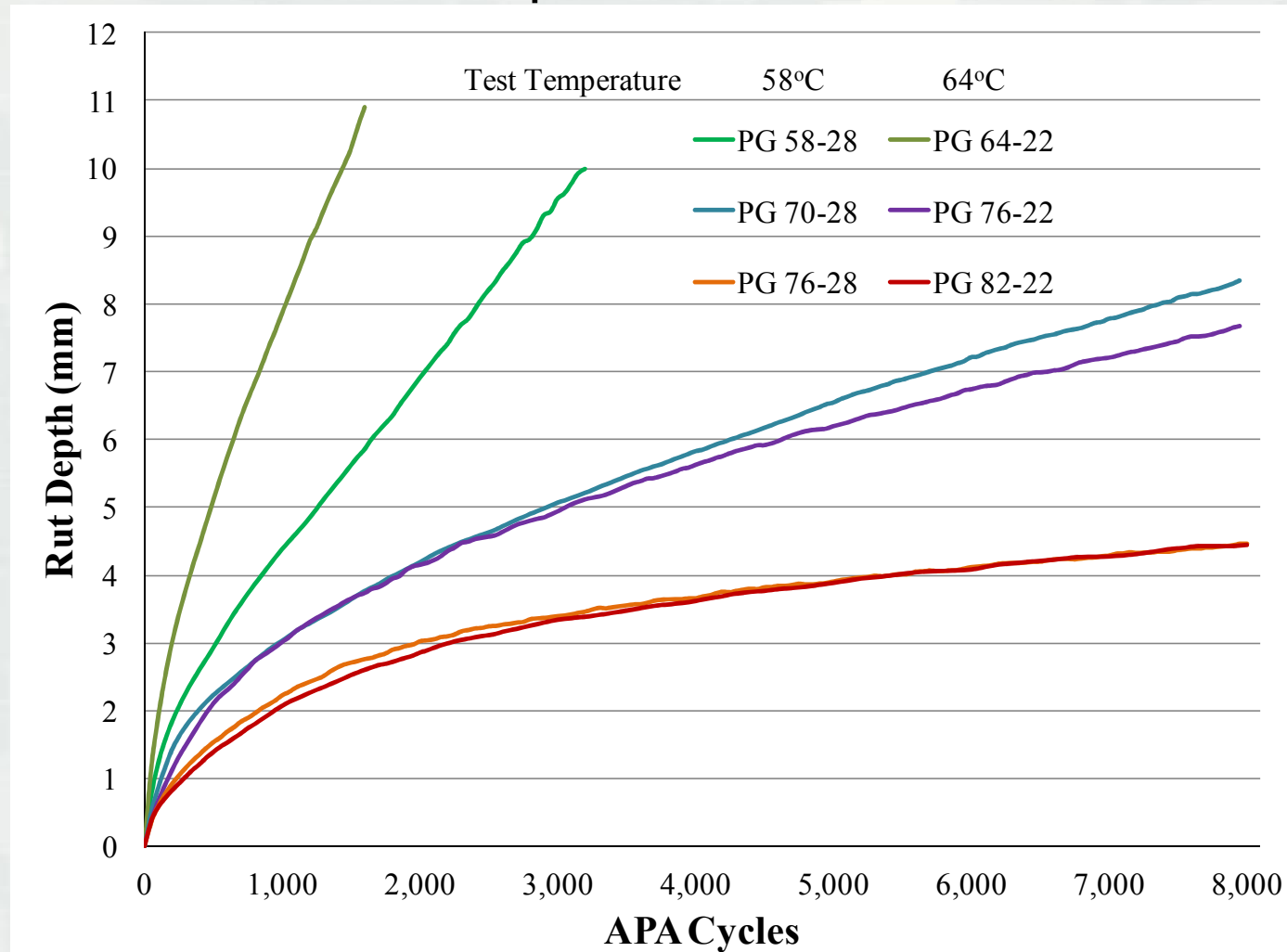
Phase 1 Results



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Influence of Binder on APA Results

Example from Phase 2



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Indirect Tensile Strength

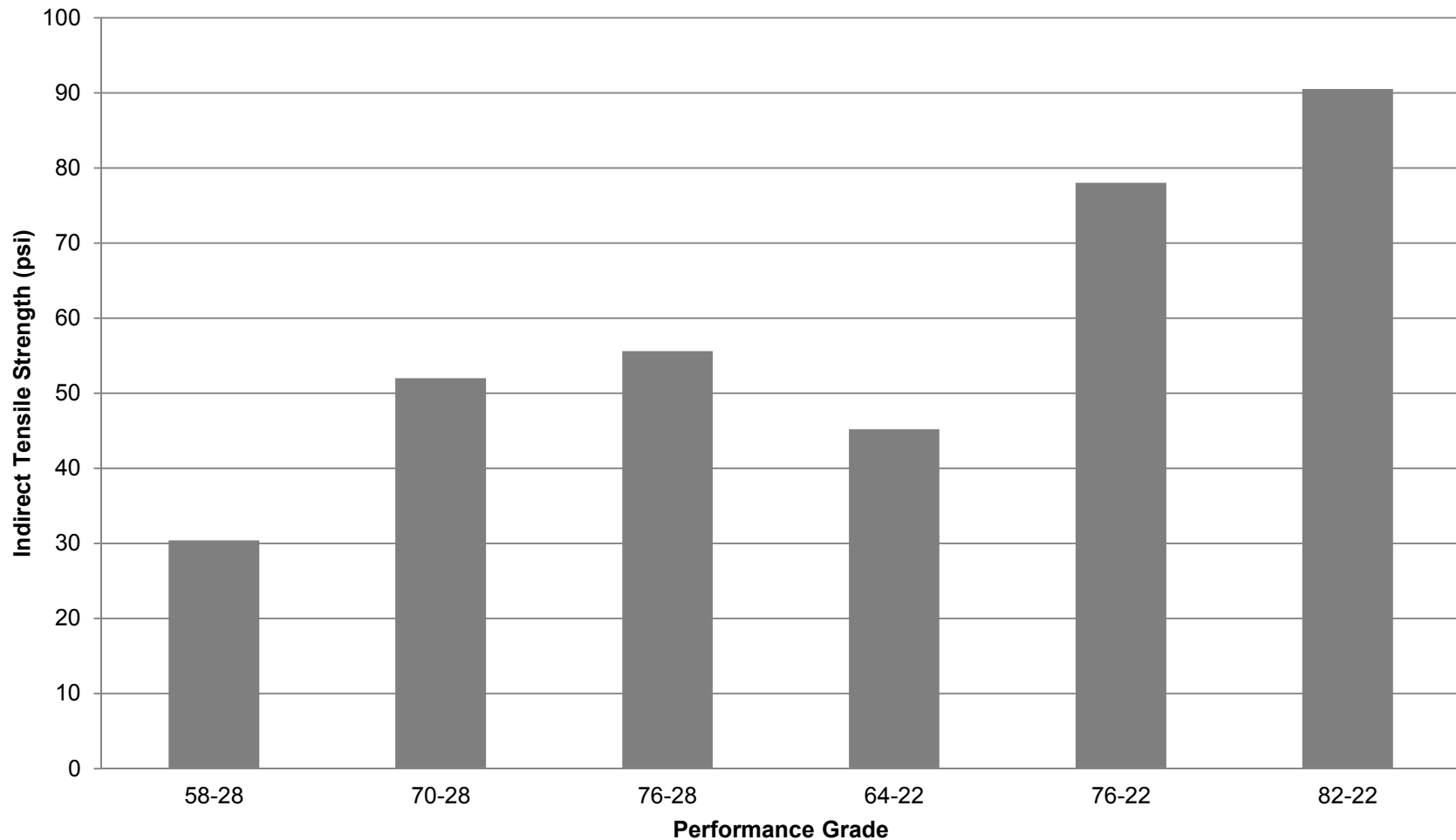
- Test performed at 40°C
- Loading rate of 50 mm/min
- Measure peak load
- Determine IDT

$$S_t = \frac{2000P}{\pi tD}$$



Influence of Binder on IDT Results

Example from Phase 2



Recommendations

- Select projects in each region and validate test acceptance thresholds for mix designs
- Incorporate performance testing requirements in next revision of AC 150/5370-10
- Use pavement management data to review field performance and relate to laboratory test data
- Conduct further investigations for using test as quality control/assurance test
 - Plant-produced mixture
 - Field cores



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Questions?

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